

ERO2.0 modelling of divertor marker erosion in ASDEX Upgrade L-mode experiments

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S. Saari^a, A. Hakola^a, J. Karhunen^a, M. Balden^b, C. Baumann^c, A. Järvinen^a, K. Krieger^b, H. Kumpulainen^c, J. Likonen^a, J. Romazanov^c, ASDEX Upgrade Team, EUROfusion^d, Tokamak Exploitation Team^e

^aVTT Technical Research Centre of Finland, Finland

^bMax-Planck-Institut für Plasmaphysik, Germany

^cForschungszentrum Jülich GmbH, Institute of Fusion Energy and Nuclear Waste Management, Germany

^dSee author list of H. Zohm et al, 2024 Nucl. Fusion <https://doi.org/10.1088/1741-4326/ad249d>

^eSee author list of E. Joffrin et al, 2024 Nucl. Fusion <https://doi.org/10.1088/1741-4326/ad2be4>



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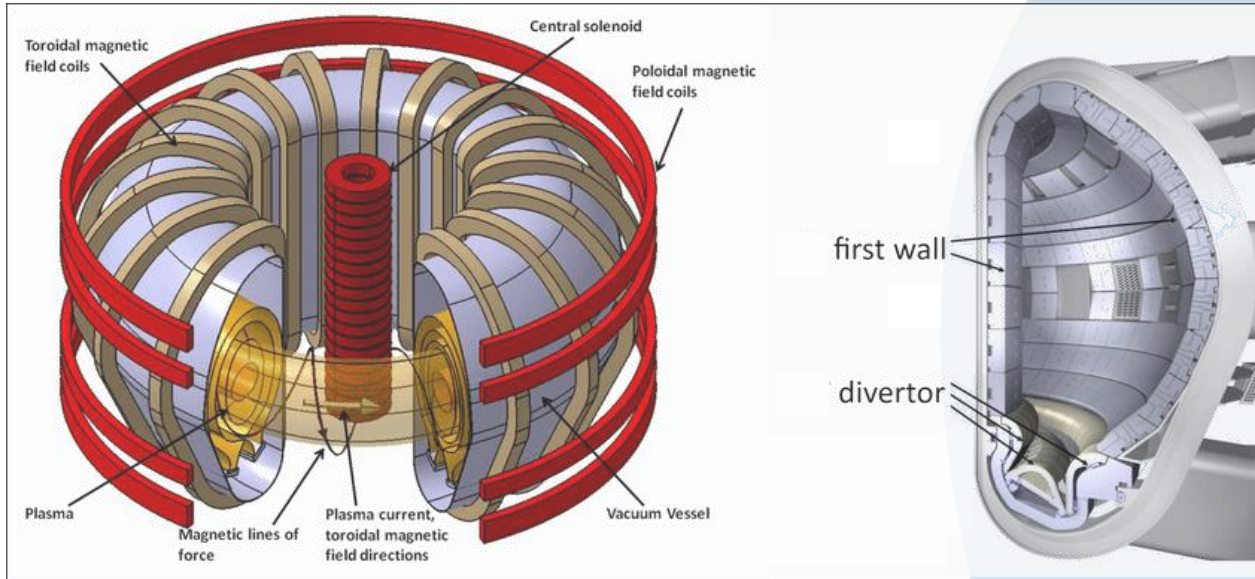


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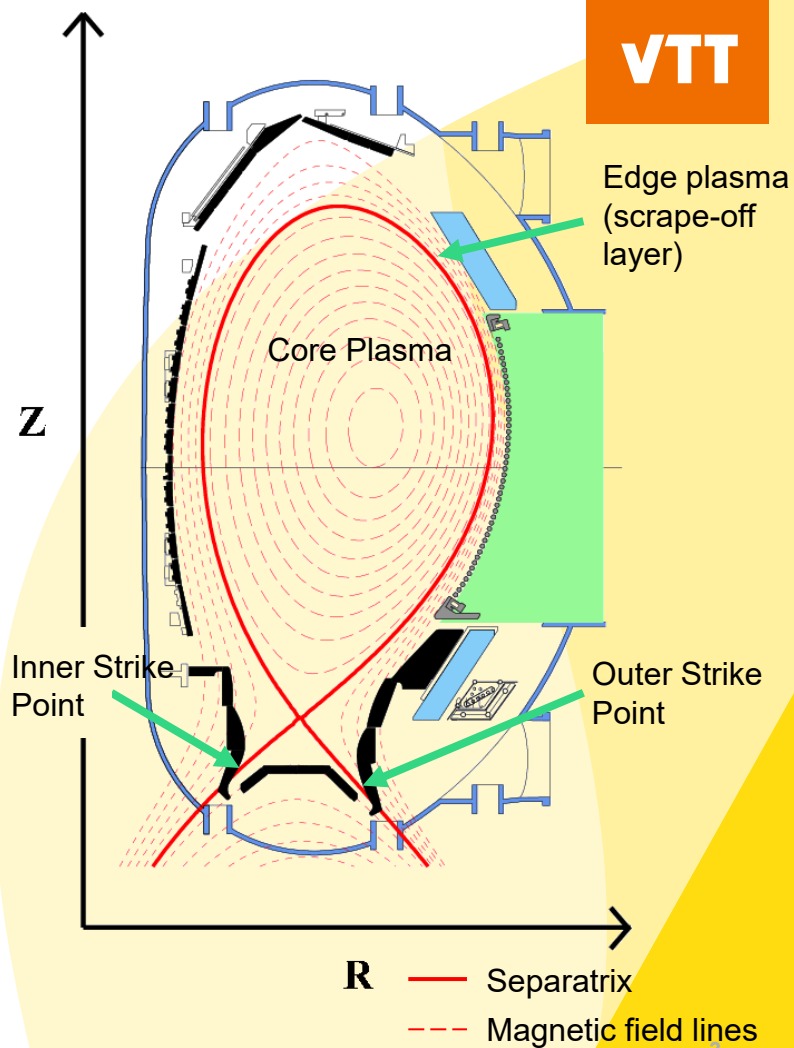
Introduction – basics of tokamak

- Most widely studied fusion reactor concept
- Plasma-state fuel (D, T) confined in a toroidal chamber with strong magnetic fields
- Temperature in the core plasma $\sim 100\,000\,000\text{ K}$



Divertor

- Plasma escaping magnetic confinement is guided along field lines to the **divertor region**
 - Field lines guide plasma to separate **divertor plates**, where it comes into direct contact with the plates
 - Ion flux and temperature are highest at the **strike point**.
 - Particles reaching the divertor are **less likely** to **return** to the main chamber or core plasma
- Although plasma is cooled in divertor prior to PFCs, it may induce sputtering

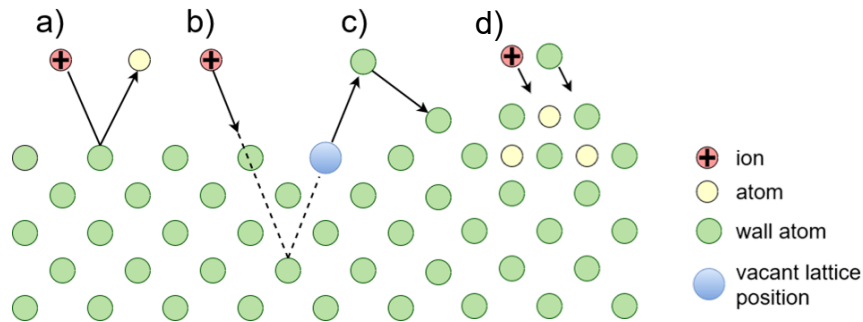


Why understanding wall erosion in tokamaks matters

- Assessing the **lifetime** of plasma-facing components (PFCs)
 - Plasma-induced erosion of wall materials significantly reduces PFCs lifespan in fusion environments
- Estimating the **amount** of wall material such as tungsten (W) **impurities** ending up in the **core plasma**
 - W, as a high-Z impurity, effectively cools the plasma through enhanced radiative losses
- **Migration** and formation of tritium (T) -containing **co-deposited layers** on the PFCs
 - D-T is favorable reaction, but due to high radioactivity and rarity of T, retention on PFCs must be minimized

Sputtering

- Incoming particle initiates collision cascade in solid leading to **ejection of atoms**
- Common **erosion mechanism** in tokamak environment
- Common PWI processes
 - a) reflection, b) sputtering, c) deposition/re-deposition, d) co-deposition



- At the divertor region PFCs particle load lead to:
 - **Gross erosion** (sputtering) of W
 - (Prompt) **re-deposition** → **net erosion** of W differs from gross erosion
 - Potential **PFC damage** (melting, cracking, etc.)

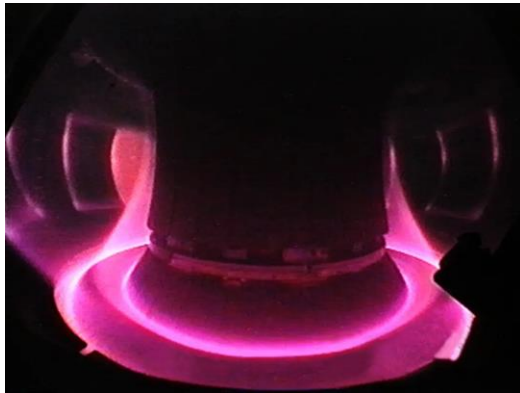
How to experimentally study wall erosion in tokamak environment [1]

- **Exposing** well-defined **samples** to controlled plasma discharges
 - Considerations for sample design:
 - Proxy material that is **separable** from surrounding materials
 - Similar **mass** and **ionization** energy as wall material
 - Sample **geometry** determines whether the study targets net or gross erosion
- Defining changes in **material thickness** through **post-mortem measurement**
 - Change in material thickness defines net erosion/deposition
 - Measurements should be material specific (RBS)
- **Simulations** help to understand physics behind the **experimental observations**

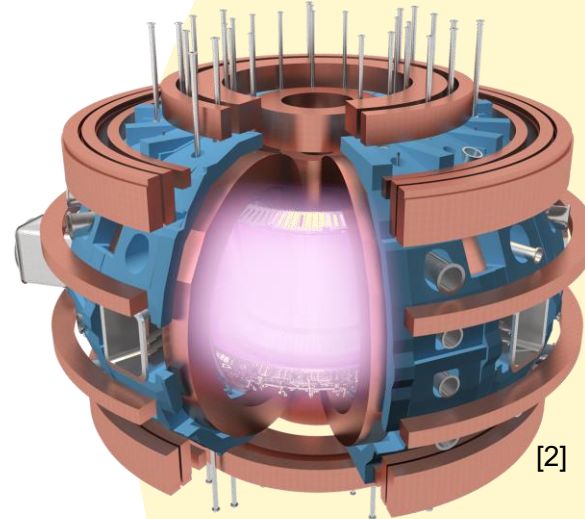
[1] R. Bastasz, et al., J. Nucl. Mater. **310–314** (1995) 220–222

ASDEX Upgrade (AUG)

- Medium-size **tokamak** located at Max-Planck-Institut für Plasmaphysik (Garching, Germany)
- Operational since 2007
- First wall equipped with **W-coated** graphite or **bulk-W** tiles



[2]

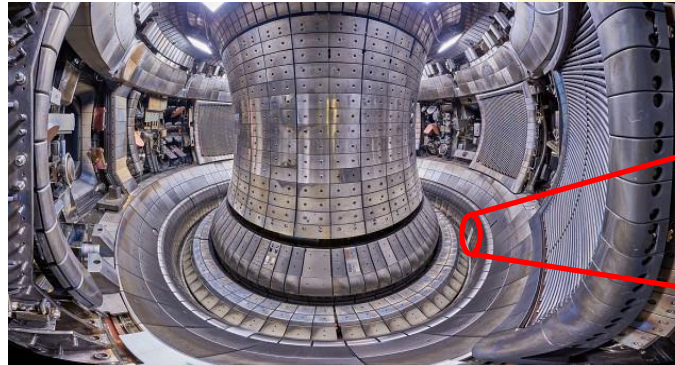
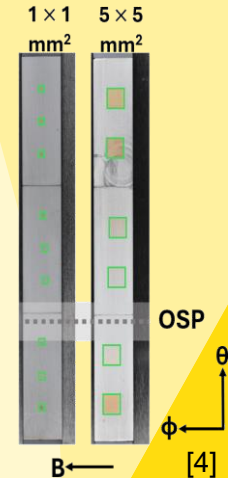
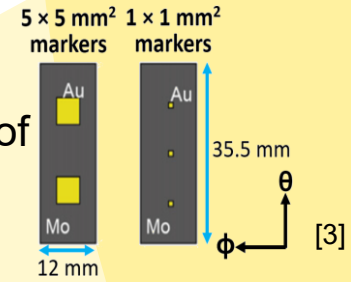


[2]

[2] IPP Online picture archive - https://www.ipp.mpg.de/1471827/asdex_upgrade

The experiment

- Mo-coated graphite samples with Au marker surfaces of two sizes ($5 \times 5 \text{ mm}^2$ and $1 \times 1 \text{ mm}^2$) were placed at outer strike point (OSP) area of AUG divertor
 - $5 \times 5 \text{ mm}^2$: re-deposition expected on marker surface → **net erosion**
 - $1 \times 1 \text{ mm}^2$: re-deposition expected outside marker surface → **gross erosion**
- Samples were subjected to 8 identical plasma discharges
 - Total exposure time: **~32 s**
 - Strike point conditions: $n_{e,OSP} \sim 0.5 \times 10^{19} \text{ m}^{-3}$, $T_{e,OSP} \sim 20 \text{ eV}$
- Main findings:
 - Erosion **peak** near **OSP**
 - Maximum **net erosion** rate **1.0-1.1 nm/s**



[3] A. Hakola et al., Nucl. Fus. **61** (2021) 116006

[4] A. Hakola et al., Nucl. Mater. Energy **25** (2020) 100863

Simulation tools

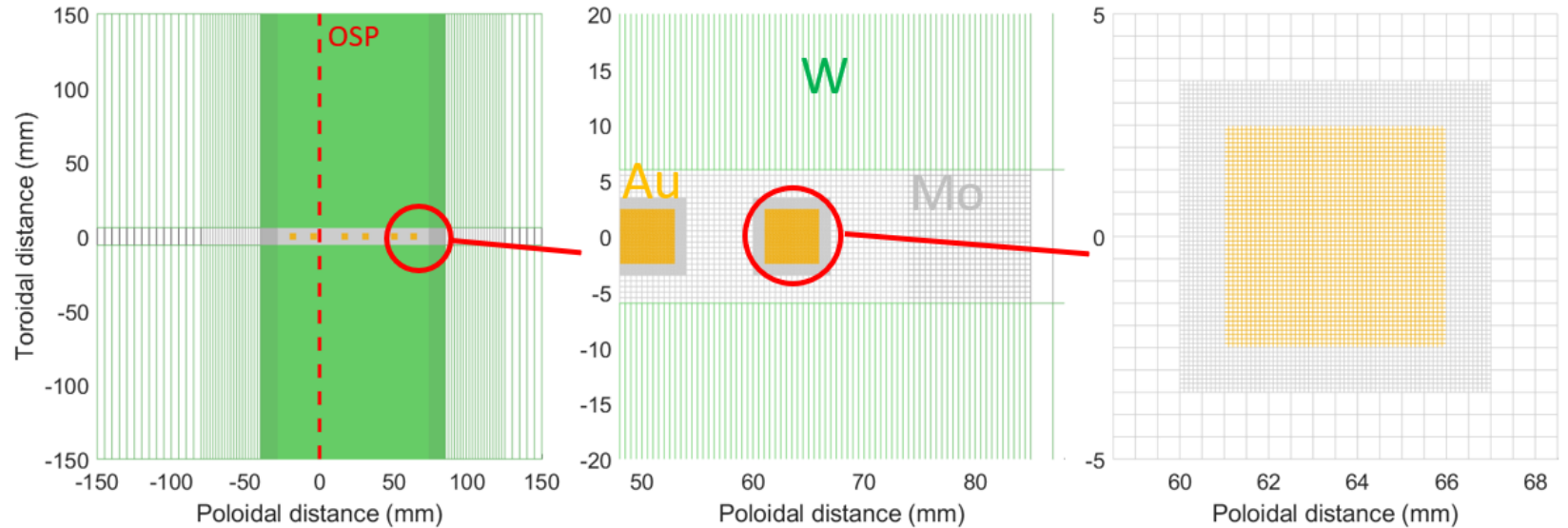
- **ERO2.0** - 3D Monte Carlo trace impurity code for modelling plasma-wall interactions (PWI) [5]
 - Upgrade to earlier ERO code
- **SDTrimSP** – Binary Collision Approximation (BCA) code to simulate atomic collisions in solid targets [6]
 - Sputtering and reflection yield data used in ERO2.0
- **OSM** – “Onion Skin Model” to produce background plasma solutions in the scrape-off layer (SOL) plasma [7]

[5] J. Romazanov et al., Phys. Scr. **T170** (2017) 014018

[6] A. Mutzke et al., SDTrimSP Version 6.00, IPP Report 2019-02

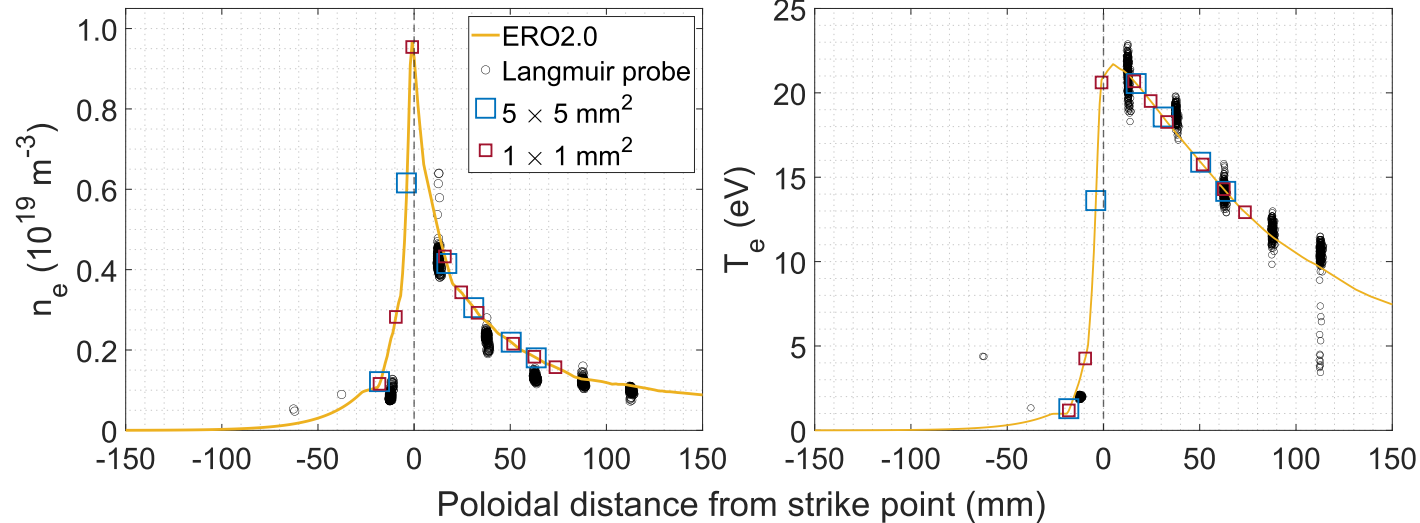
[7] P. Stangeby, et al., Nucl. Fusion **35** (1995) 1391.

Simulation geometry



- Simulation volume **$300 \times 300 \times 50 \text{ mm}^2$**
- Poloidal-toroidal surface along outer target plate constructed from **rectangles** with decreased sizes in areas of interest

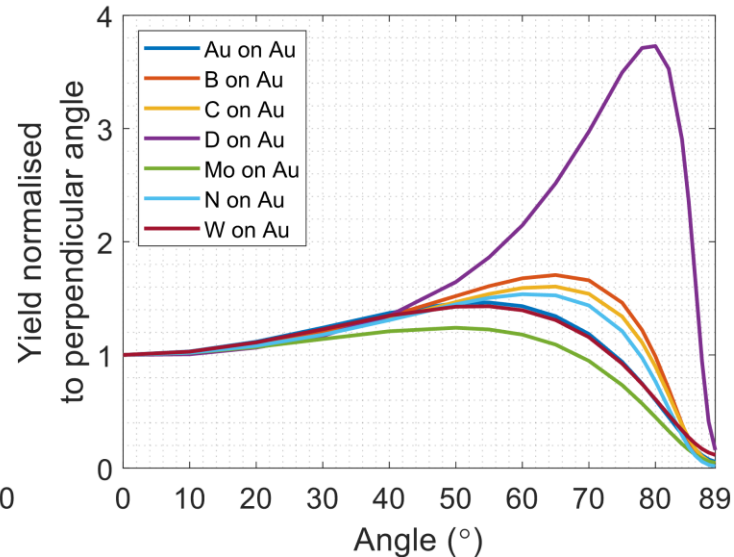
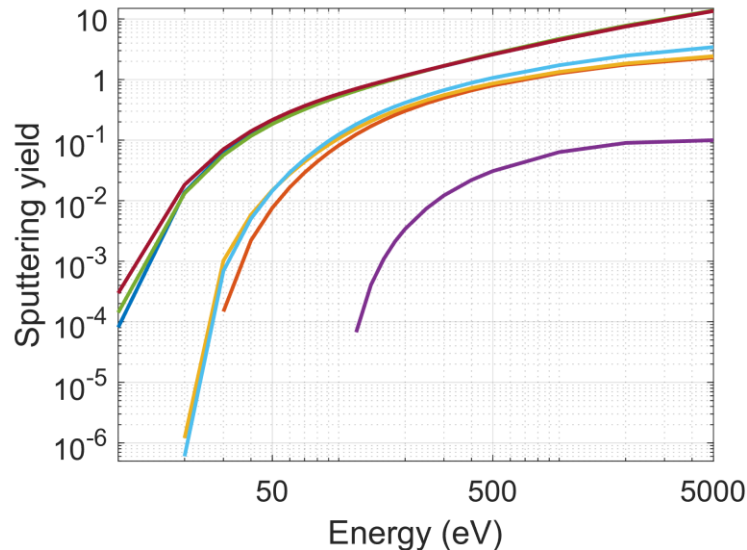
Background plasma and parameters of simulation



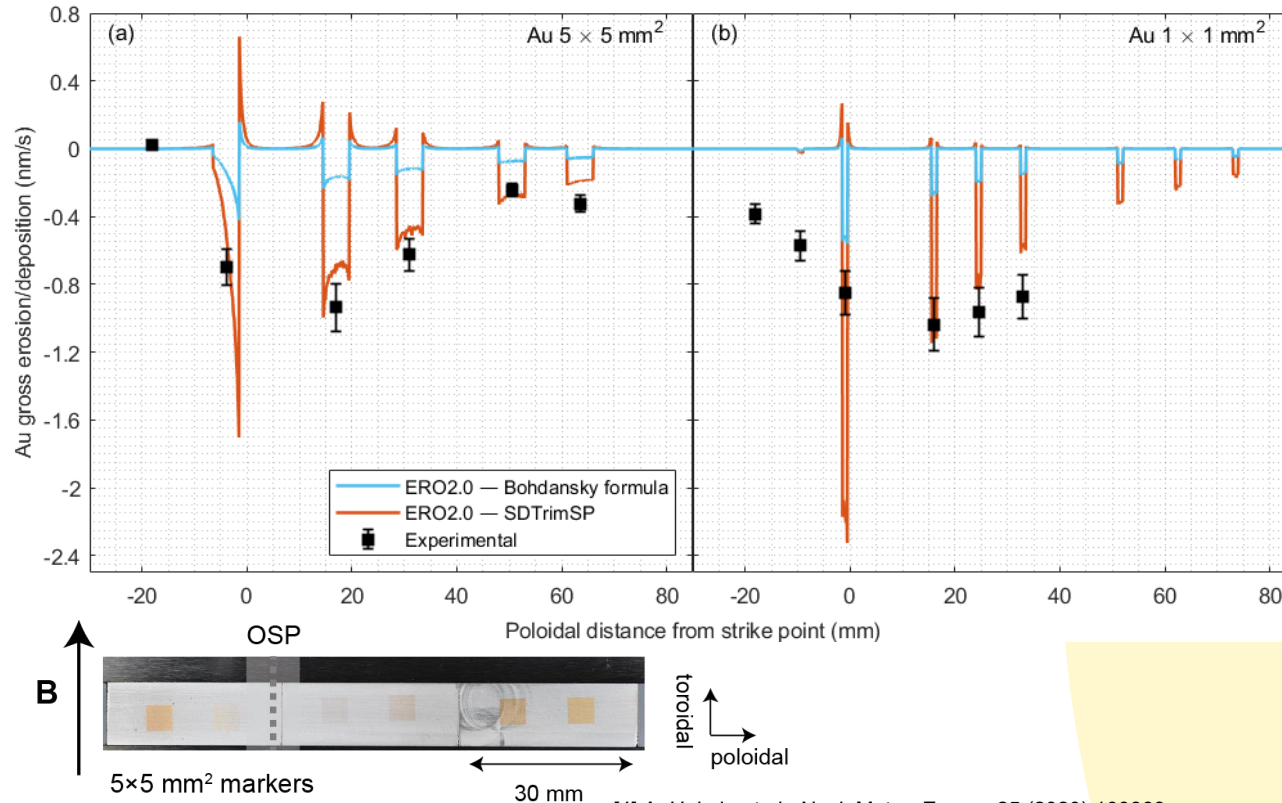
- Applied background plasma created with OSM follows the Langmuir-probe (LP) measurements of electron density and temperature at the outer divertor target [3]
- Spatially homogenous constant impurity concentrations of $c_B = c_C = c_N = 0.5\%$ and $c_W = 0.005\%$, with average charge states $Z_B = 3$, $Z_C = 4$, $Z_N = 5$, $Z_W = 13$ [4]

Sputtering data

- Angle dependent erosion and reflection data for Au computed using **SDTrimSP**
- Angle dependent results are compared to previously used sputtering yields provided by the **Bohdansky formula** with no angle dependency [4]

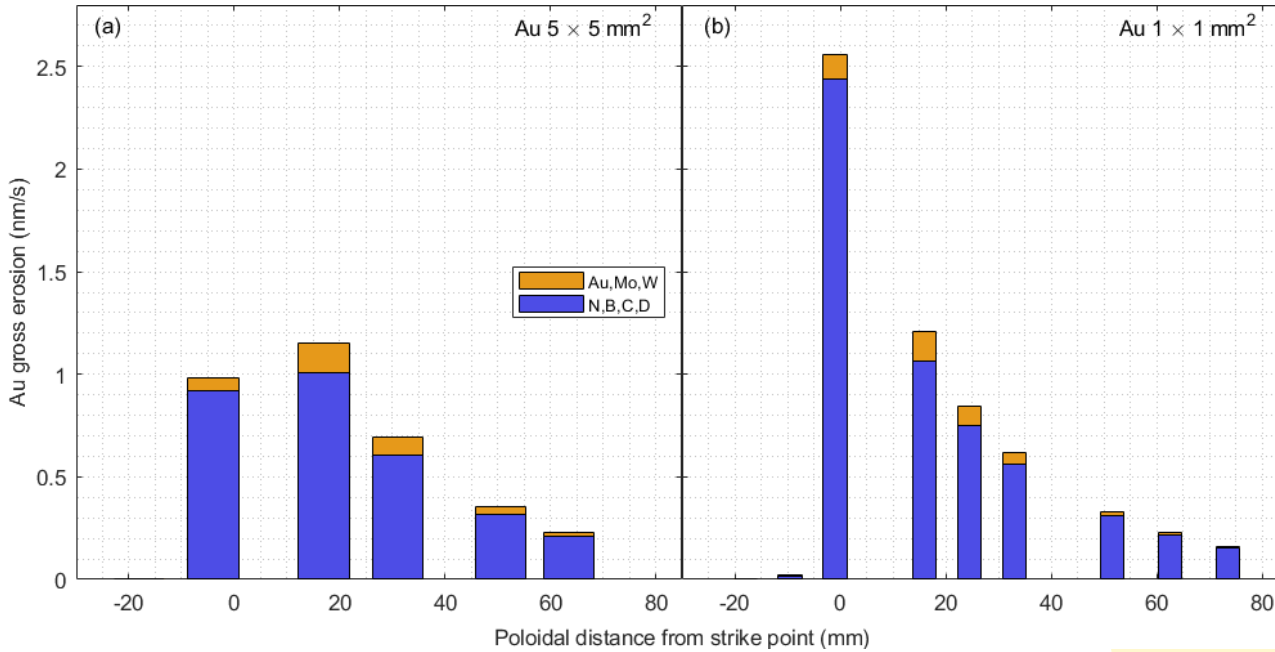


Net erosion of Au markers reproduced reasonably well in ERO2.0 simulations with new SDTrimSP sputtering data



- Significantly improved match to measured net erosion of Au with new SDTrimSP data with respect to estimates given by the Bohdanský formula
- Deviations around OSP and PFR arise from (i) uncertainties in location of OSP and absence of LP data in its immediate surroundings, (ii) shape of n_e and T_e profiles in the PFR and (iii) experimental uncertainties

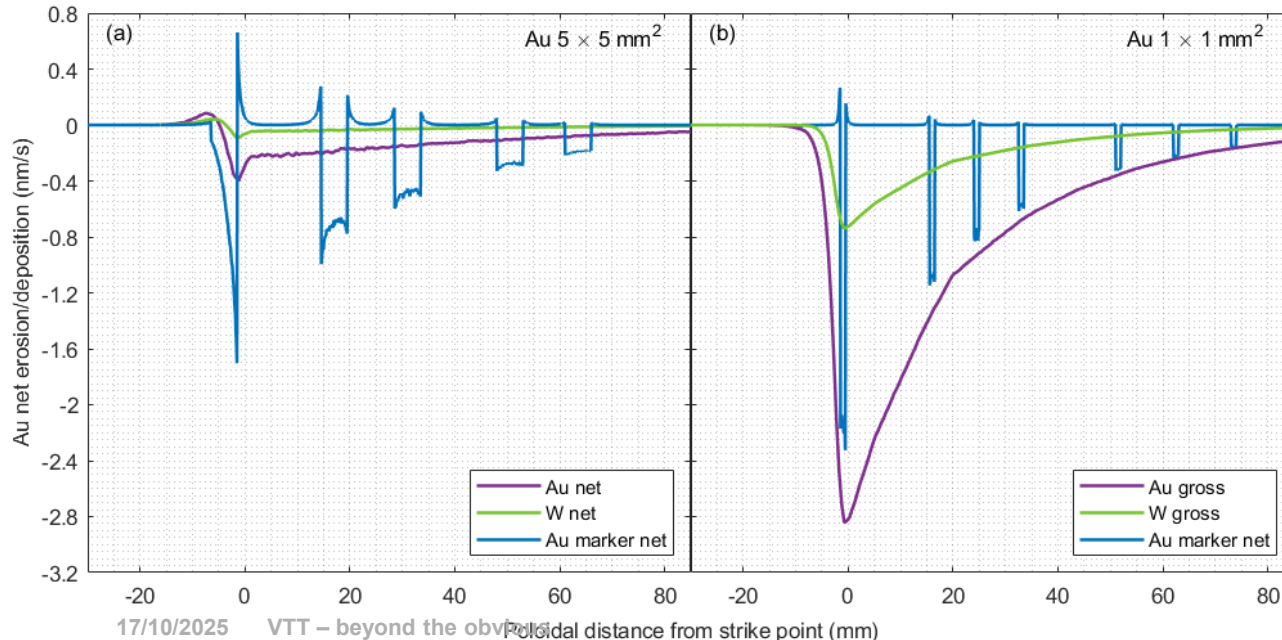
The effect of different impurities on gross erosion



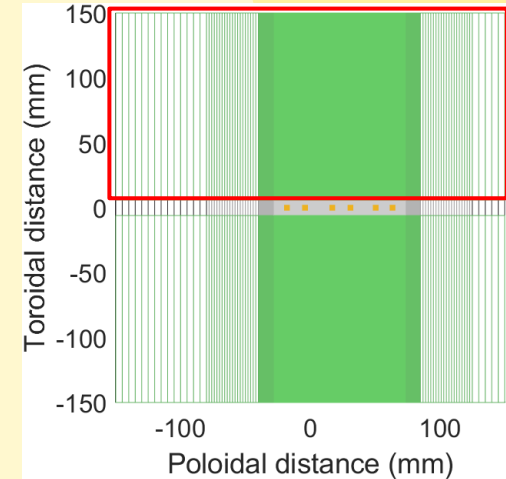
- **Gross erosion** of surfaces is primarily driven by **light B, C, and N impurities**
 - Simulation sensitive to impurity concentration → calls for further studies
- Eroded Au, Mo, or W have **minor role** in sputtering
 - Eroded material **promptly re-deposited** as low-energy particles

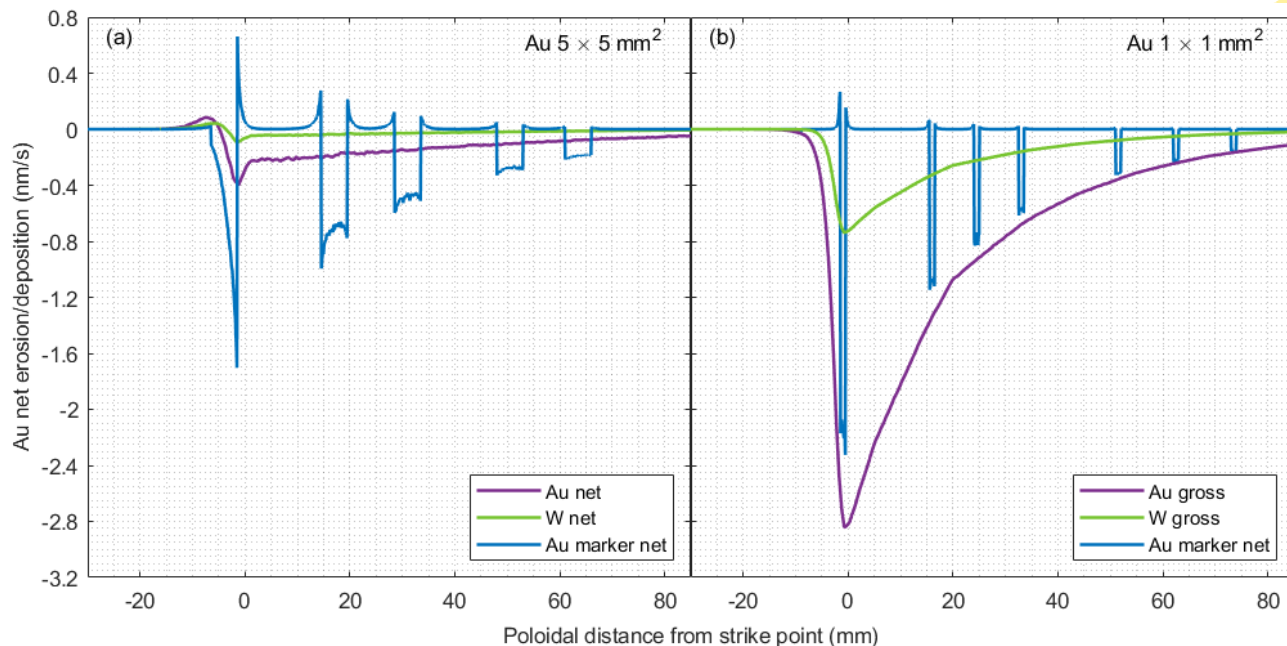
Au as proxy for W

- Net erosion of **toroidally extended Au** surfaces (fig. a) **3—6 times higher** in comparison to **W**
- **Gross erosion** of **toroidally extended Au** surfaces (fig. b) **4—6 times higher** in comparison to **W**
→ Au erosion substantially higher in comparison to W. **Au suboptimal** proxy for quantitative assessment of **W erosion**



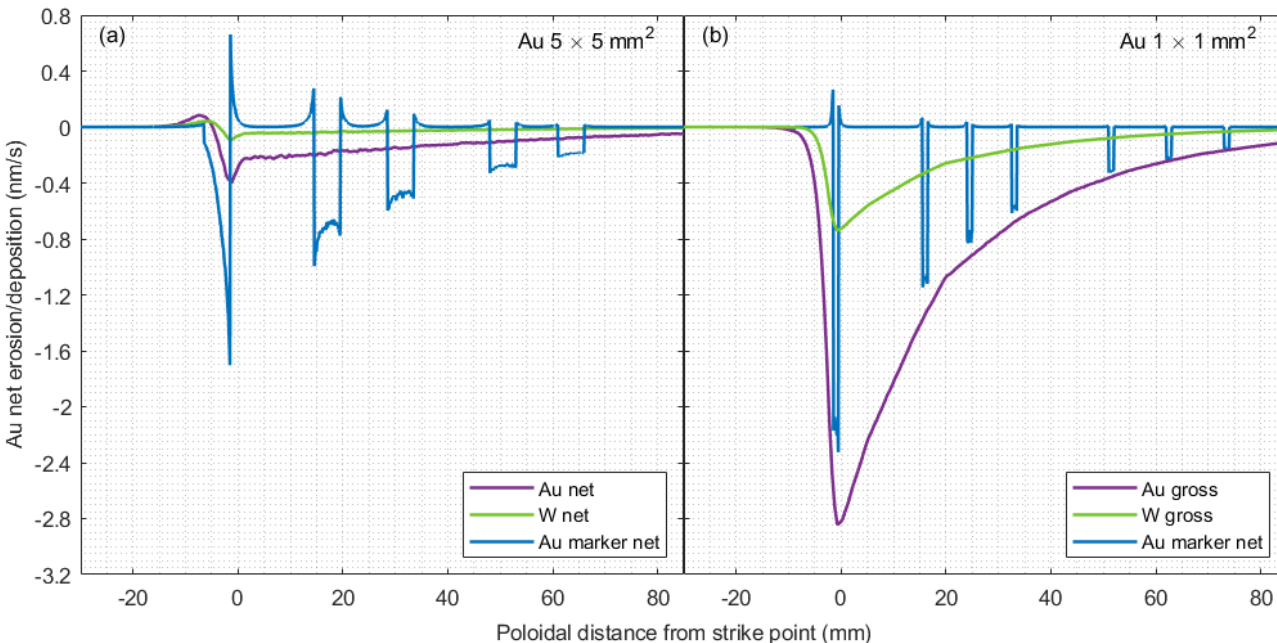
Toroidally extended Au/W surface (changed from W to Au in some simulations)





- **Net erosion of $5 \times 5 \text{ mm}^2$ markers 2—6 times higher** in comparison to **toroidally extended Au** surfaces
→ $5 \times 5 \text{ mm}^2$ markers **too small in toroidal direction for net erosion studies** due to re-deposition of eroded Au largely toroidally downstream from the marker surfaces

Au as proxy for W



- Agreement within 20% between net erosion of $1 \times 1 \text{ mm}^2$ Au markers and gross erosion of toroidally extended Au surfaces
→ $1 \times 1 \text{ mm}^2$ markers suitable for gross erosion studies

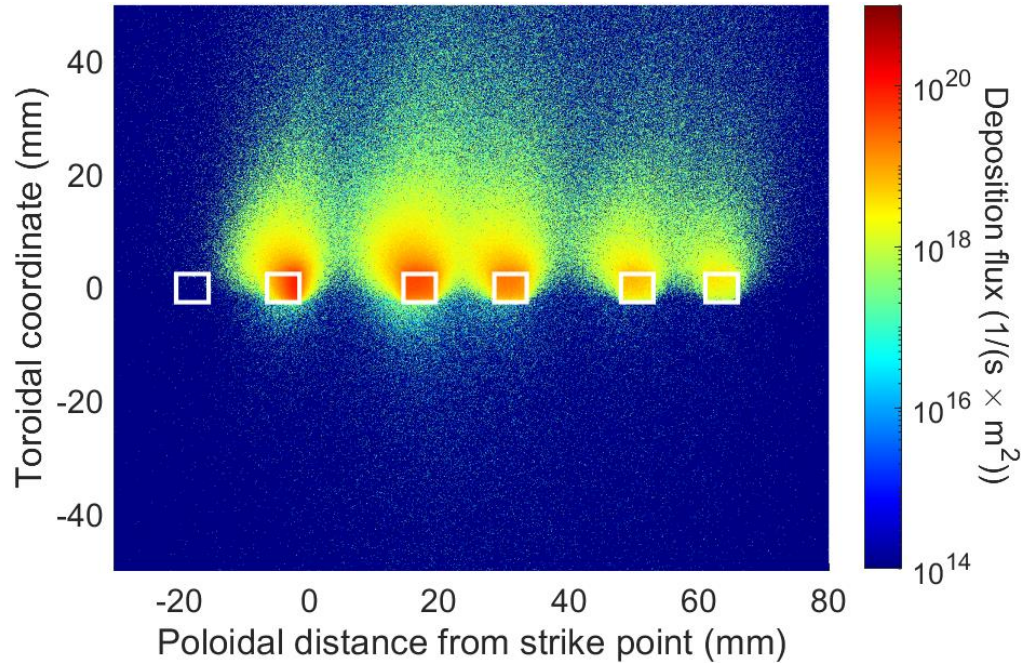
⇒ Net and gross erosion of W overestimated by factors of 15–20 and 3–4 by Au markers due to material and geometry effects

Conclusions

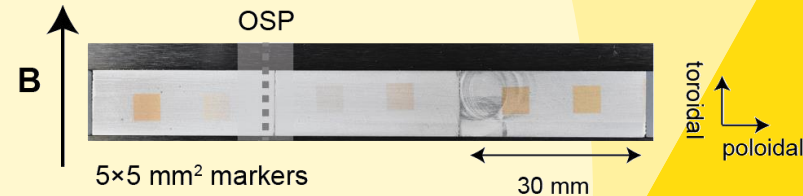
- ⇒ Erosion of Au markers near the outer strike point of AUG simulated using ERO2.0 and SDTrimSP
- ✓ Improved agreement between simulated and measured net erosion of Au particularly due to adoption of new sputtering and reflection data created with SDTrimSP
 - ✓ Net erosion was found to be caused mostly by light impurities of the background plasma
 - ✓ Au was found to be a poor proxy for quantitative assessment of W erosion; $5 \times 5 \text{ mm}^2$ markers too small in toroidal direction for studying net erosion.
 - New experiments are needed with better proxy materials, such as Pt, and improved marker geometries for net erosion studies

Backup slides

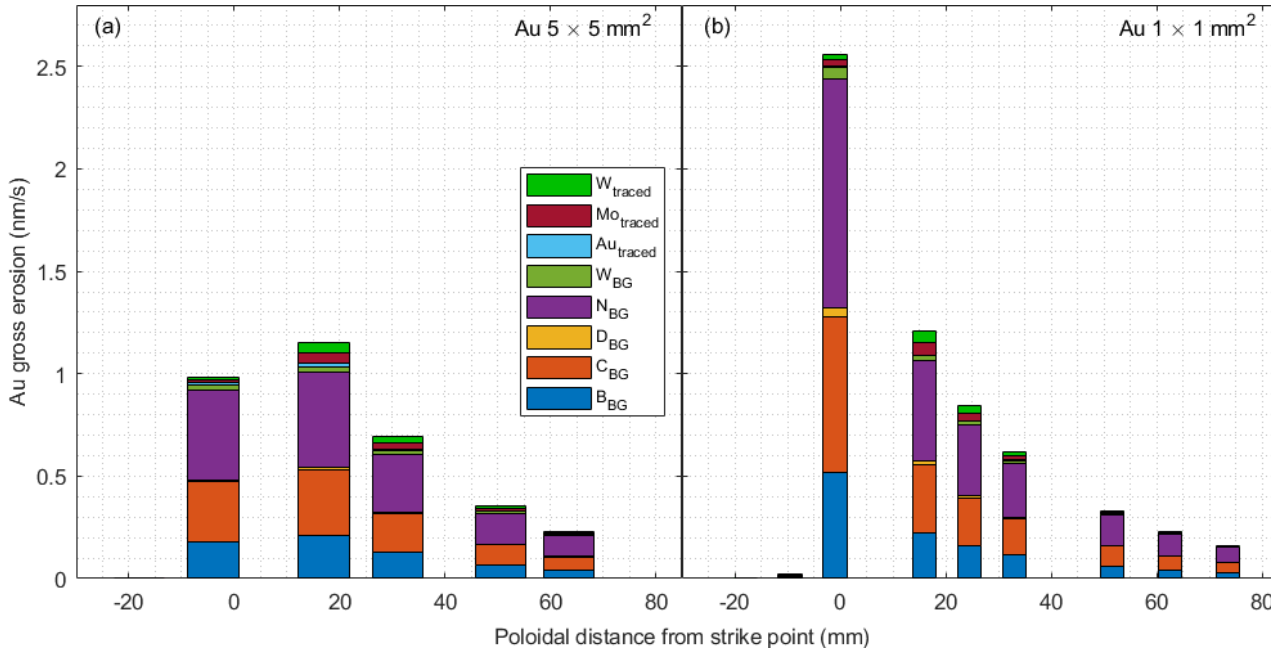
Deposition of particles



- Narrow net **deposition peaks** next to markers due to **re-deposition** of material eroded from marker **edges**
- **Migration of particles** is primarily in the **toroidal direction**



Impact of impurities



- **Gross erosion** of surfaces is primarily driven by **light B, C, and N impurities**
 - Simulation sensitive to impurity concentration → calls for further studies
- Eroded Au, Mo, or W has **minor role** in sputtering
 - Eroded material **promptly re-deposited** as low-energy particles