

# Impact of Fuel Type and Discharge Burnup on Spent Fuel Properties

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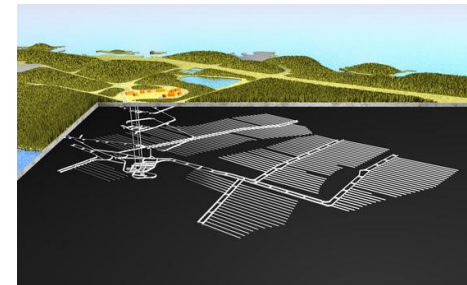
1.11.2019 VTT – beyond the obvious

## Motivation and context 1/2

§ Knowledge of spent nuclear fuel (SNF) properties is important in SNF management, e.g.:

- Decay heat and reactivity determine the repository space needed for SNF disposal.
- Nuclide inventories are needed for safe handling of SNF and estimates of dose released to the biosphere.

§ Accurate knowledge of SNF properties (source term) and associated uncertainties yield savings in repository space and enhanced safety.



Source: Posiva Oy

## Motivation and context 2/2

- § This work is part of a larger effort to establish methods to computationally determine the SNF source term by studying
- computational uncertainties related to the determination of the spent fuel source term and
  - **effect of different fuel types and burnups on the source term.**
- § Calculations are done with the Monte Carlo code Serpent 2 [1].
- § The work is carried out in the KYT2022 project KÄRÄHDE.

[1] Leppänen, J., et al. (2015) "The Serpent Monte Carlo code: Status, development and applications in 2013," *Ann. Nucl. Energy*, 82 (2015) 142-150.



Source: Posiva Oy

## Background

§ Similar calculations performed at VTT in 2005 [2] with SCALE-5 package

- VVER-440: 3.7 and 4.0 wt-% U-235 enrichment
- BWR: 3.8 and 4.2 wt-% U-235 (0, 40 and 80 % void fraction)
- EPR: 3.6 and 4.0 wt-% U-235

§ Decay heat, activity, photon source strength, etc. for 40, 50 and 60 MWd/kgU discharge burnup

§ Decay heat production for 20, 30, 40, 50 and 60 MWd/kgU discharge burnup

[2] Anttila, M. "Radioactive Characteristics of the Spent Fuel of the Finnish Nuclear Power Plants", Posiva Working Report 2005-71

# New round of calculations in KYT2022/KÄRÄHDE

§ New codes (Serpent) & nuclear data

§ Additional fuel types

Phase 1:

| Parameter                             | BWR GE14<br>(10 x 10) | VVER-440 TVEL<br>2 <sup>nd</sup> gen | EPR<br>(17 x 17) | VVER-1200 |
|---------------------------------------|-----------------------|--------------------------------------|------------------|-----------|
| U-235 Enr. (%)                        | 4.23                  | 4.37                                 | 3.60             | 4.92 (*)  |
| Normal rods                           | 74                    | 120                                  | 253              | 306       |
| Gd rods                               | 18                    | 6                                    | 12               | 6         |
| Gd <sub>2</sub> O <sub>3</sub> (wt-%) | 3 or 8                | 3.35                                 | 9                | 5         |
| Boron (ppm)                           | 0                     | 500                                  | 600              | 600       |

(\*) 0.7 % U-236  
included

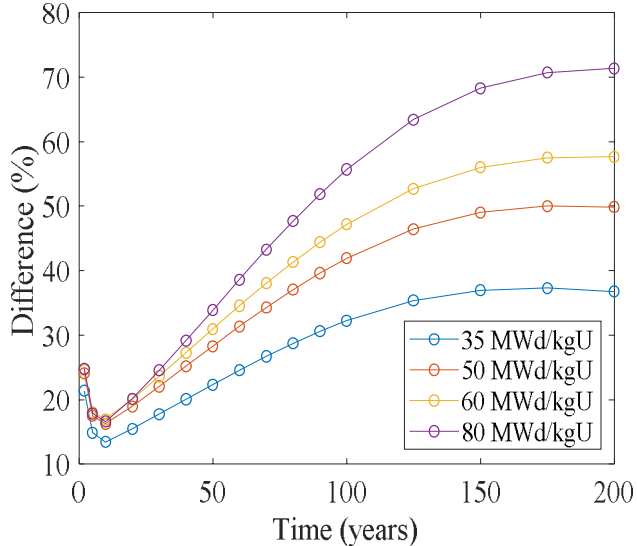
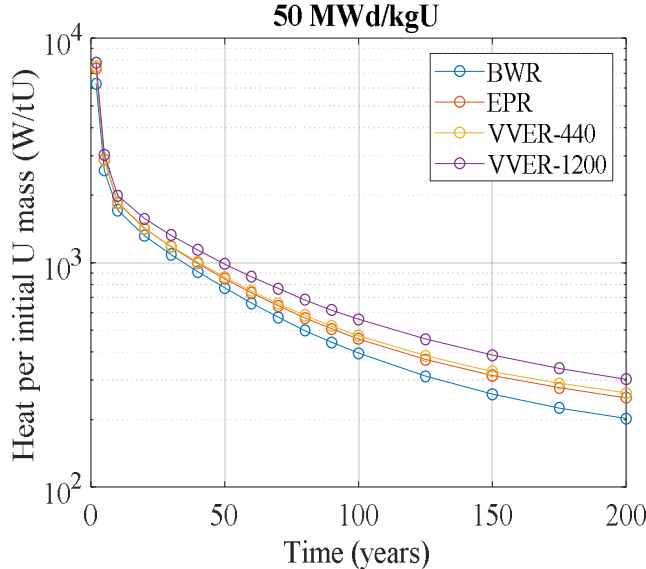
## Computational model

- § Serpent 2.1.31 with JEFF-3.2 cross-section and JEFF-3.1.1 fission yield & decay data
- § 2D Monte Carlo burnup calculation, reflective or periodic boundary conditions
- § All models up to 80 MWd/kgU, intermediate burnup data written to restart file at several burnup points
- § Short burnup steps
  - 0.1 – 0.3 MWd/kgU to Xe-equilibrium
  - 0.5 MWd/kgU to peak reactivity (full depletion of Gd)
  - 2.5 MWd/kgU later
- § For several discharge burnup, decay calculations to  $10^7$  years after discharge

A decorative pattern on the left side of the slide, composed of a grid of triangles in various shades of blue, with some triangles in white and green.

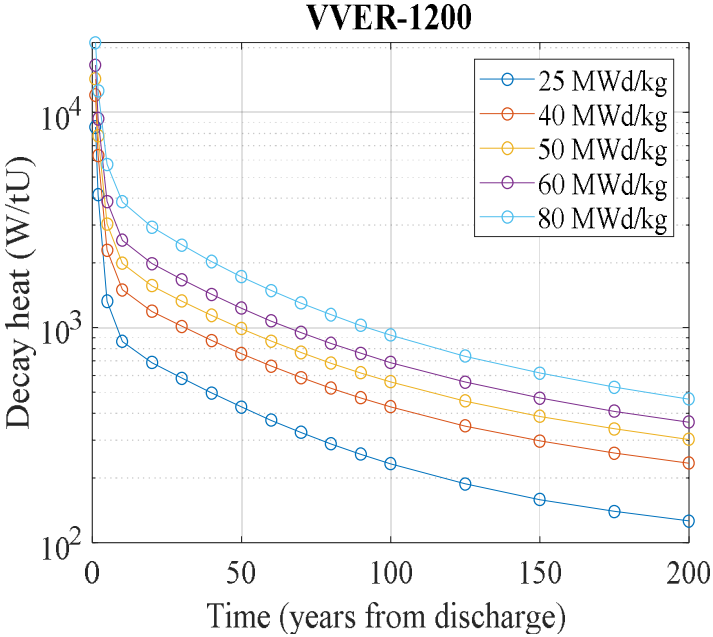
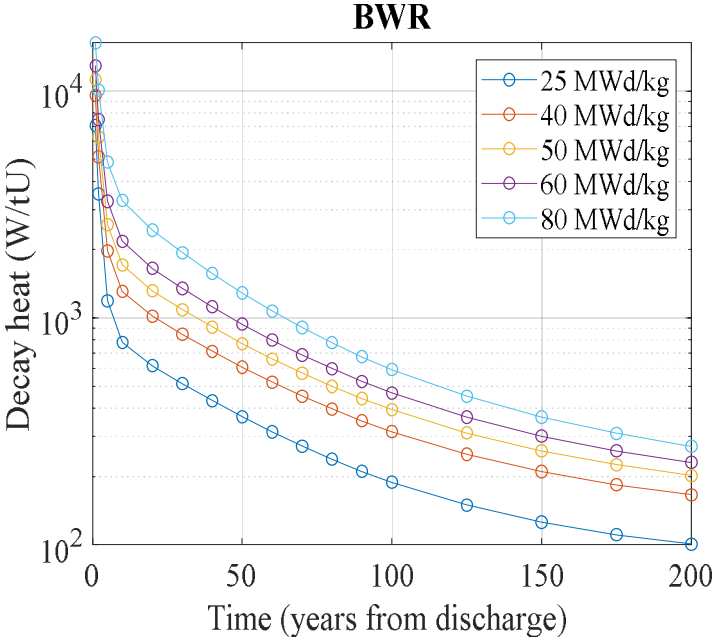
# Results

# Decay heat – fuel type comparison



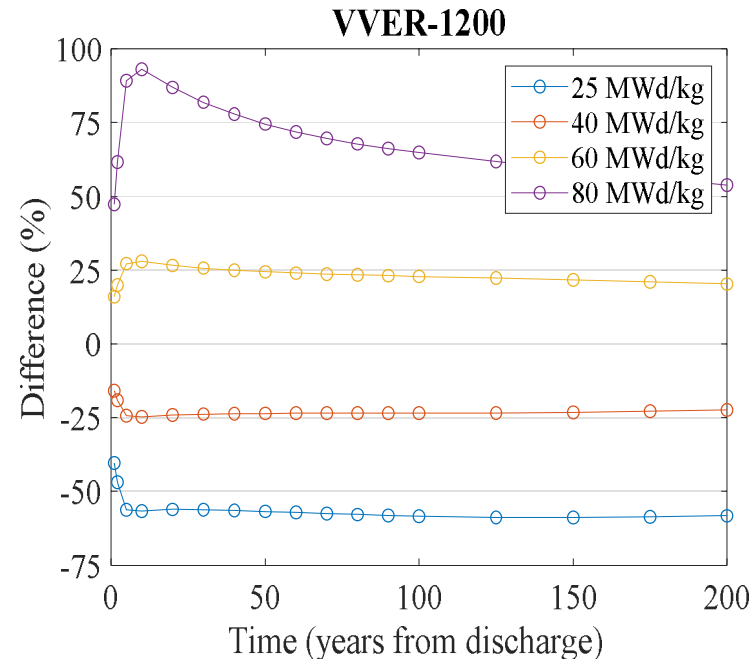
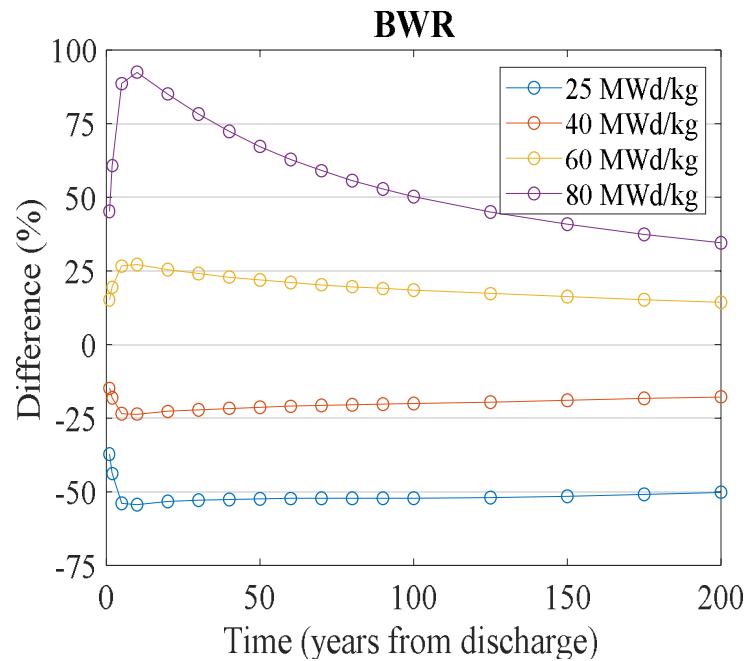


# Decay heat – burnup comparison



# Decay heat – burnup comparison (rel.)

Reference 50 MWd/kgU

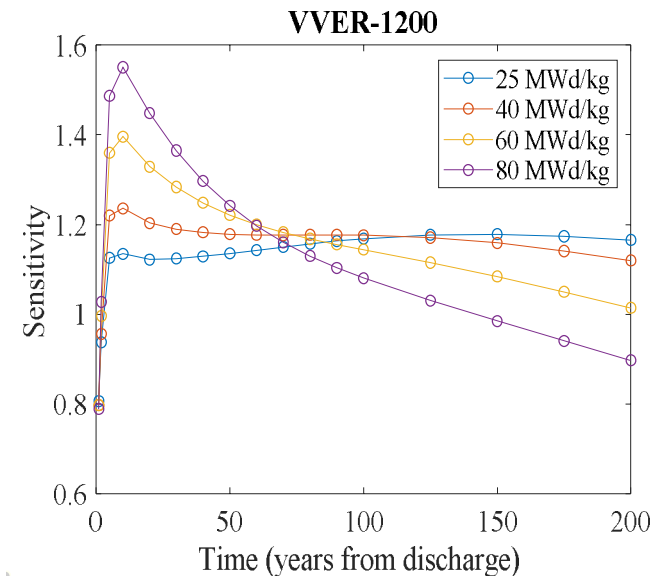
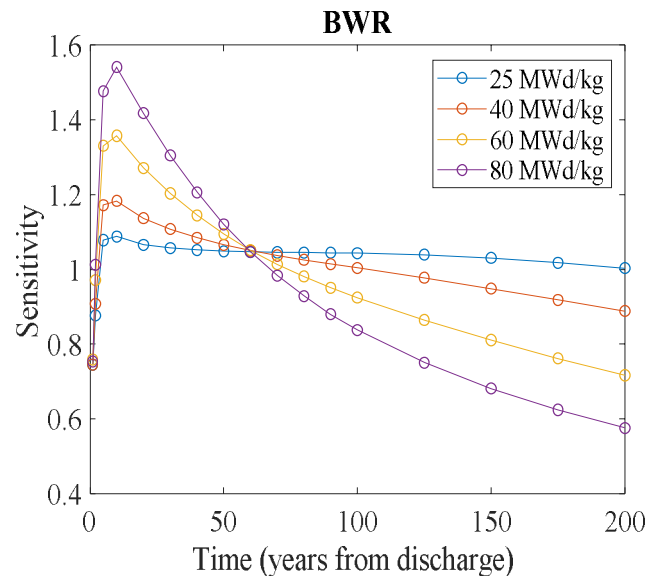


# Decay heat – sensitivity to discharge burnup

$$S = \frac{H_i - H_{BU\_ref}}{H_{BU\_ref}} \cdot \frac{BU_{i-} - BU_{ref}}{BU_{ref}}$$

$BU_{ref} = 50 \text{ MWd/kgU}$

$H = \text{decay heat}$



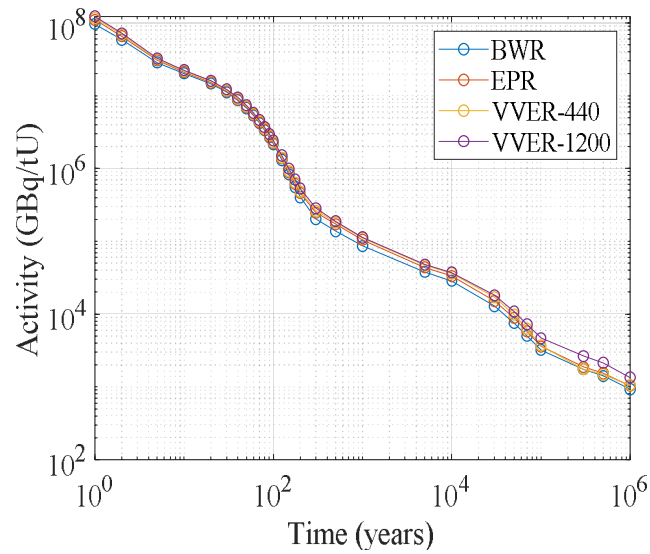
## Top decay heat contributors 5 years after discharge

| BWR    | %    | EPR    | %    | VVER-440 | %    | VVER-1200 | %    |
|--------|------|--------|------|----------|------|-----------|------|
| Y90    | 27.7 | Cs134  | 27.2 | Cs134    | 27.9 | Cs134     | 25.4 |
| Ba137m | 27.2 | Ba137m | 24.5 | Y90      | 25.2 | Y90       | 24.2 |
| Cs134  | 24.9 | Y90    | 23.2 | Ba137m   | 25.1 | Ba137m    | 23.2 |
| Cm244  | 10.2 | Cm244  | 13.7 | Rh106    | 11.4 | Pu238     | 16.9 |
| Rh106  | 10.0 | Rh106  | 11.4 | Cm244    | 10.3 | Rh106     | 10.4 |

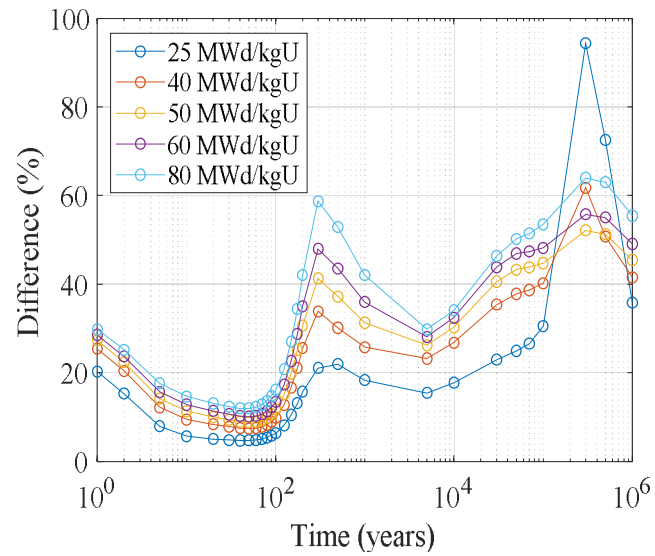
## Top decay heat contributors 100 years after discharge

| Nuclides | % (BWR) | % (EPR) | % (VVER-440) | % (VVER-1200) |
|----------|---------|---------|--------------|---------------|
| Am241    | 40.0    | 44.8    | 46.4         | 39.1          |
| Pu238    | 22.8    | 23.6    | 22.6         | 34.8          |
| Ba137m   | 16.3    | 14.1    | 13.6         | 11.4          |
| Y90      | 15.0    | 12.1    | 12.4         | 10.7          |
| Pu240    | 5.9     | 5.4     | 5.0          | 4.0           |

# Total activity

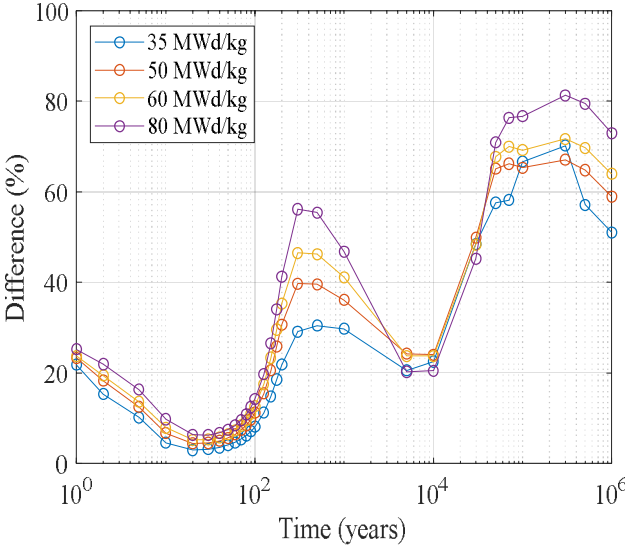
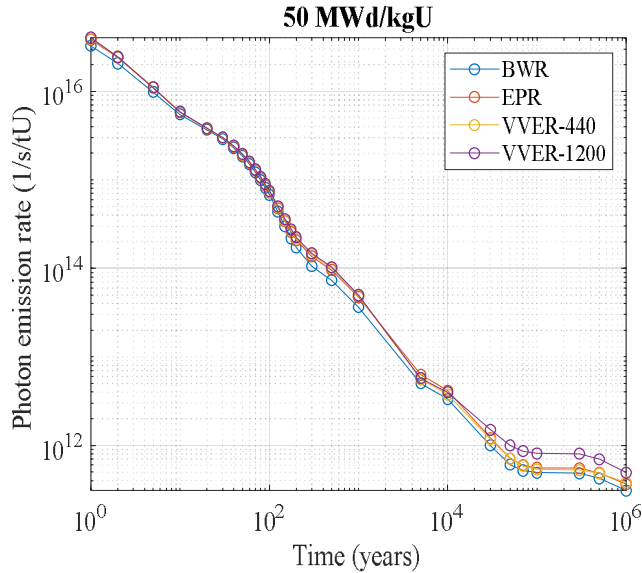


Discharge burnup 50 MWd/kgU



Relative difference between the most and least active assembly

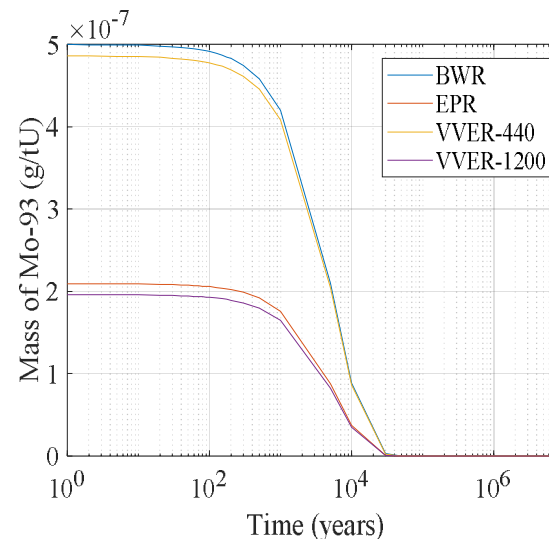
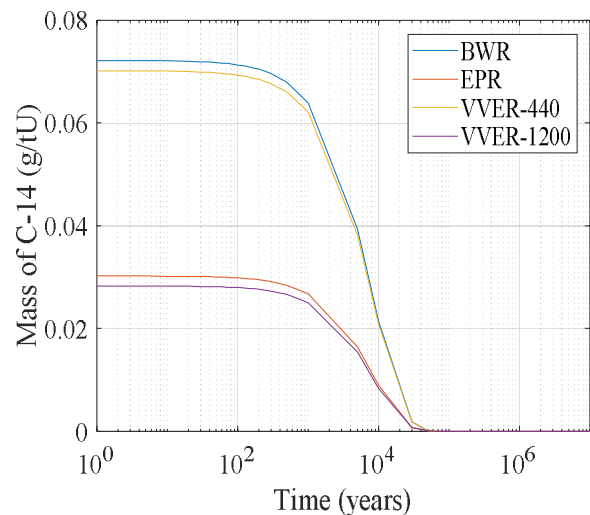
# Photon emission rate



Relative difference between the most and least active assembly

# Migrating nuclides

C-14, Cl-36, Mo-93, Ag-108m and I-129 determined to be the most likely to propagate to biosphere from repository



← 50 MWd/kgU discharge burnup



## Summary, conclusions & future

- § 2D Monte Carlo burnup calculation performed with Serpent for a fuel assembly representing BWR, EPR, VVER-440 and VVER-1200, approximated irradiation history
  - Differences identified, significance for each application to be determined in separate analyses
- § More fuel types to be calculated in 2020-
  - E.g. other types of BWR assemblies with various void fractions
  - Effect of burnup, enrichment, amount of burnable absorbers, etc. on larger variety of source term components (such as spontaneous fission, plutonium mass,...)